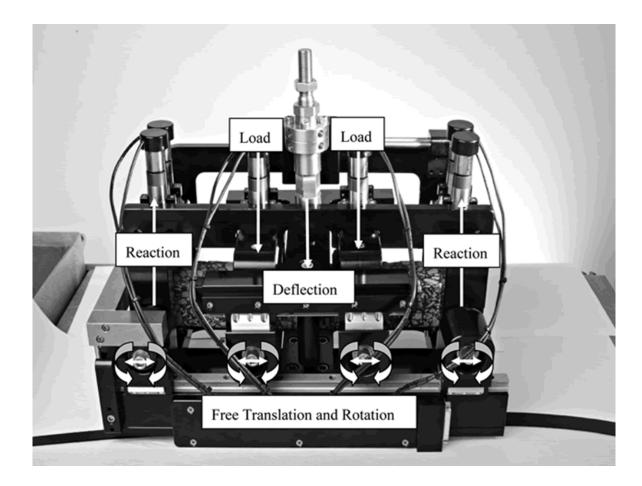
Difference Between Fixed and Floating Reference Points

AASHTO

T-321

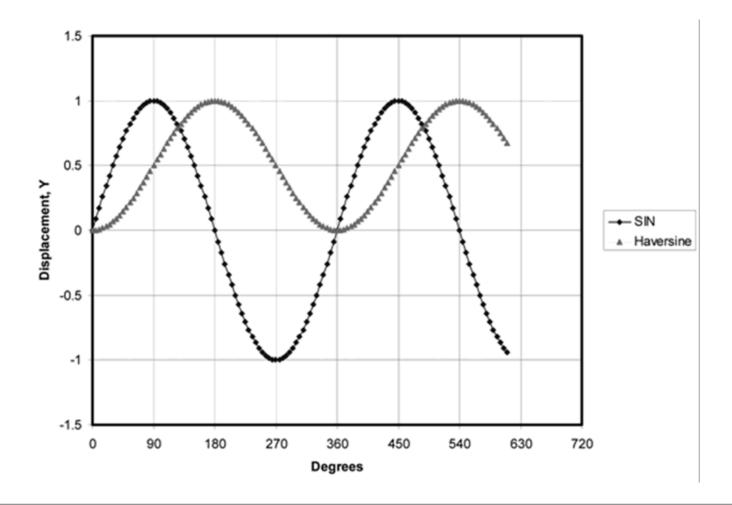


Fixed Reference LVDT with Target Attached to the Beam Neutral Axis (Mid-Height, Mid-Length)



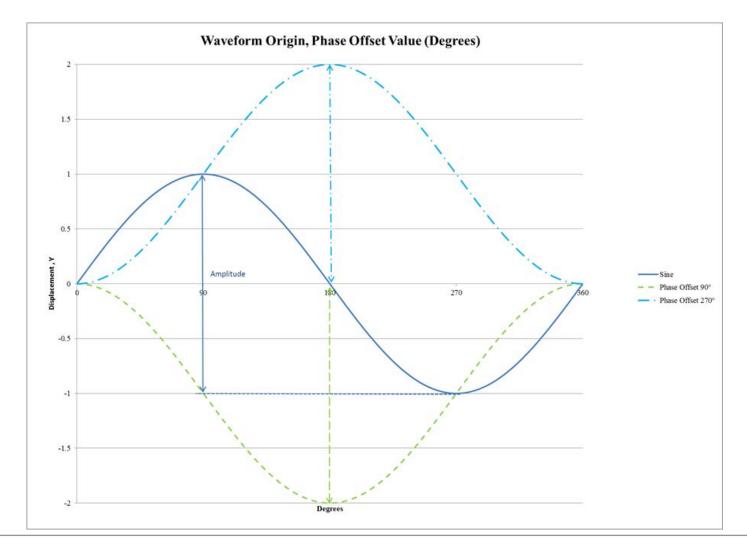


Old ASTM D7460 Graph Improper Representation of Equipment Response



MWV

New ASTM D7460 Graph of Wave Response

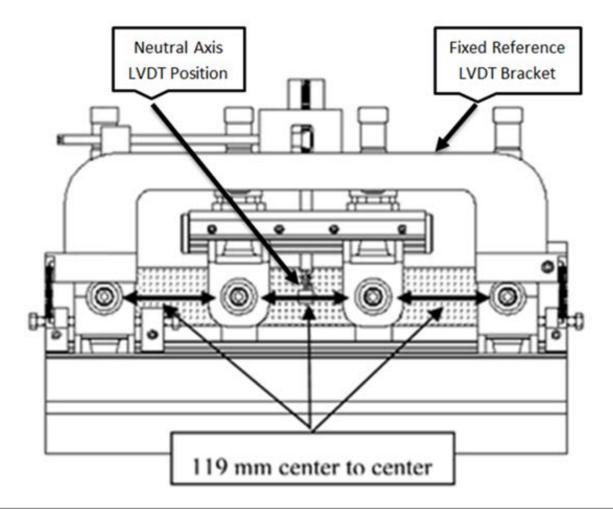




Sinusoidal Waveforms @ 90° & 270° Phase Offsets Comparison Fixed vs. Floating Reference Points

FRM-006					[Waveform Origin, Phase Offset Value (Degrees)
Beam Fat	tigue Testir	g Summa	ary							1
10 Hz, 15	C	-								
				Target	Actual	Report		Normalized		
		Level	Initial	Amplitude	Amplitude	Amplitude		Modulus		
		of	Beam	Calculated	at 50th	at 50th	Test	Failure		
	Air Voids	Micro	Stiffness		Cycle	Cycle	Termination	Point		
Beam	(%)	Strain	(MPa)	(mm)	(mm)	(mm)	(cycles)	(cycles)		
(FRM-006I	D) UTM (Do	wn)Fixed	Ref-Point	L (357)	L (357)	L (357)			(FRM-006D) UTM (Down)Fixed Ref-Point	
1	5.1	2000	1928	1.0721	1.0721	N/A	980,000	646,160	Mean Stand Dev COV	
2	4.6	2000	1928	1.0949	1.0949	N/A	1,300,000	848,920	570,550 158,993 28	
3	4.7	2000	1804	1.0888	1.0888	N/A	1,900,000	421,720	Removed the high and low values	
4	3.6	2000	1851	1.0766	1.0766	N/A	560,000	348,320		
5	3.2	2000	1866	1.0784	1.0784	N/A	1,100,000	757,640		
6	3.5	2000	1295	1.0776	1.0776	N/A	640,000	456,680		a the second
Average	4.1		1779	1.0814	1.0814					
(FRM-006	E) UTM (Up)	-Fixed Re	ef-Point	L (357)	L (357)	L (357)			(FRM-006E) UTM (Up)-Fixed Ref-Point	
1	2.9	2000	2004	1.0607	1.0607	N/A	920,000	646,880	Mean Stand Dev COV	
2	3.1	2000	1942	1.075	1.075	N/A	1,600,000	882,560	674,360 189,682 28	
3	3.1	2000	1940	1.0748	1.0748	N/A	920,000	738,120	Removed the high and low values	Deflection Deflection
4	3.6	2000	1933	1.0883	1.0883	N/A	560,000	347,240		
5	3.5	2000	1886	1.0896	1.0896	N/A	1,500,000	926,640		
6	3.3	2000	1915	1.0706	1.0706	N/A	800,000	429,880		
Average	3.3		1937	1.0765	1.0765					
				δx►Target	δχ=½δς	δc				
(FRM-006	G) Floating	Ref-Point	t (UP)	L/6 (237)	L/6 (237)	L (Calc)			(FRM-006G) Floating Ref-Point (UP)	
1	3.9	2000	1606	0.5357	0.5372	1.0743	2,521,550	1,634,300	Mean Stand Dev COV	
2	3.2	2000	1220	0.5377	0.5356	1.0712	2,304,000	1,278,390	1,127,143 166,251 15	
3	3.1	2000	1682	0.5344	0.5335	1.067	1,426,130	901,570	Removed the high and low values	
4	3.6	2000	1875	0.5357	0.5366	1.0731	2,134,080	633,380		
5	3.4	2000	1916	0.5356	0.534	1.0681	1,749,220	1,220,860		
6	3.4	2000	1841	0.538	0.5385	1.0769	1,849,460	1,107,750		
Average	3.4		1690	0.5362	0.5359	1.0718				

Fixed Reference LVDT Flexural Beam Fatigue Test Apparatus, Side View



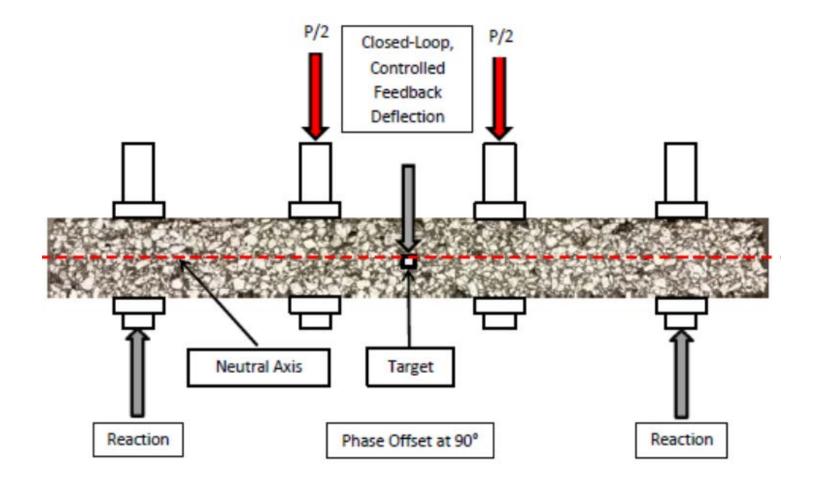
Fixed Reference LVDT

Fixed reference linear variable differential transducer (LVDT) closed loop controlling on a flexural beam fatigue (FBF) is defined as referencing the FBF frame that is bolted to the base plate. The LVDT is affixed to a free floating horizontal translation bar contacting three guide bearings on the outer fixed frames. Springs are used to stabilize the L-shaped bar from jumping the track and lifting off the bearings. The tension from the springs keep tension on the bar minimizing any variability in the LVDT readings as the test is being performed. The design makes no contact with the beam being tested other than the internal spring tension of the LVDT used to measure displacement.

- Reference point is fixed and never changing from cycle one throughout FBF test
- LVDT is referencing the target that is affixed to the neutral axis of the beam (½ the height & ½ the length of the beam)
- Equation in both ASHTO T-321 and ASTM D7460 reference the neutral axis for calculations

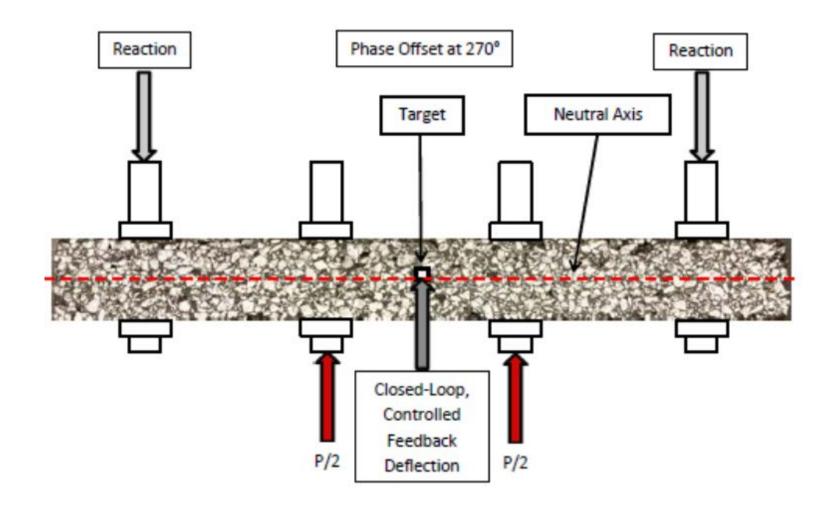


Load Characteristics of Fatigue Test Apparatus Illustrated at 90° Phase Offset



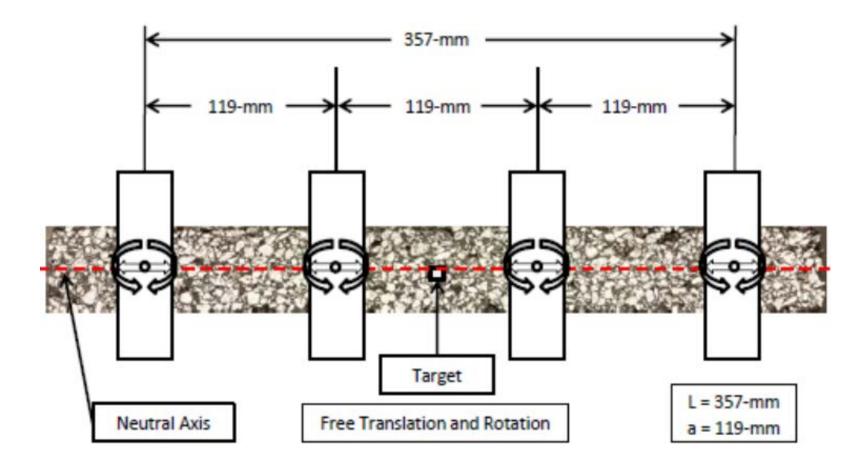


Load Characteristics of Fatigue Test Apparatus Illustrated at 270° Phase Offset

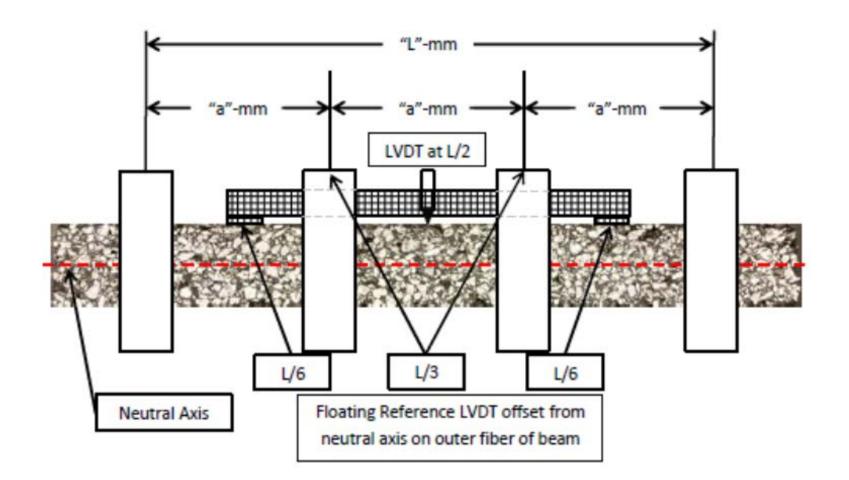


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Diagram of Free Translation and Rotation Specified in Both AASHTO T-321 & ASTM D7460



Floating Reference LVDT with Targeting on Top of Beam to Tension Side of Beam displacement



MWV

Floating Reference LVDT

Floating reference LVDT on a FBF is defined as referencing the beam at the length between the outside frames divided by 6 (L/6). The L/6 location is $\frac{1}{2}$ the distance between the outside frames and inside frames on a 4-point beam fixture.

- Reference point constantly changing through the duration of the test
 - Referencing the same object that you are breaking down
 - Pre-calculated displacement for the equation is changing due to the free floating reference point at the L/6 position.
 - Reference point is affected by multiple variables in a mix design
 - Aggregate size
 - Aggregate shape (flat, round, elongated, etc.)
 - Aggregate porosity
 - Binder grade
 - Reference point is affected by specimen response due to:
 - Temperature selection during FBF test
 - Mix design sag between the outside and inside clamps due to gravitational effects
 - Friction values of mix design during FBF testing
- LVDT is referencing the top of the beam
 - > LVDT beam referenced location is in violation of AASHTO T-321-03 Section 8.2
 - > Tensile side of beam when ran at 270° phase offset
 - Compressive side of beam when ran at 90° phase offset



- Equation in AASHTO T-321-03 reference the neutral axis for calculations
 - Offset of ½ the distance from the neutral axis is not calculated for in the FBF equation in AASHTO T-321-03 section 9.1.2
 - > Measurement of tensile and compression side of beam are different lengths
- Fabricator specific issues
 - Some old equipment without the repair of free horizontal translation on the H-frame
 - Beam specimen is being improperly strained between all clamping frames
 - > Pendulum design for free horizontal translation at the two outside fixed frames
 - Estimated minimal variability, but it is additive
 - > Applied motor force at each frame
 - Average force of motors
 - Area of clamp pads on sample
 - Average force per mm²
- Operator specific issues
 - Running beam intentionally through zero
 - SHRP A-404 9.2.2 states: "The loading applied imparted tension only at the extreme fiber." (One direction loading)
 - Different operation of running beams through zero when measuring the contact points on the top or bottom of the beam weather you are fixed or floating will give you different values
 - Forcing beams through zero also induces healing, because you are putting energy back into the beam to compress what you have just stretched
 - Reduction in strain on beams being tested through zero is due to ½ strain tensile ½ strain compressive



Combined Issues with Horizontal Fixtures

- Controller is not capable of referencing the origin start position once the test is initiated
 - H-Frame floats from its point of origin
- Horizontal beams will always have sagging between frames due to the viscoelastic nature of asphalt mixtures.
 - H-Frame lifts due to movement of L/2 origin start position during test until asphalt mixture in beam plateaus
 - Movement prior to start of test waiting for temperature stabilization



Thank you.

